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An Employee-Owned Company

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Sincerely,


TABLE 1: ALLOWABLE DESIGN STRESS FOR Ultralam ${ }^{\text {TM }}$ LVL ( psi$)^{1,2}$

| PROPERTY |  | 2.0E | 1.8 E |
| :---: | :---: | :---: | :---: |
| Modulus of Elasticity $($ MOE $)$ | Joist | $2,000,000$ | $1,800,000$ |
|  | Plank | $2,000,000$ | $1,800,000$ |
| Flexural stress-MOR $\left(F_{\mathrm{b}}\right)^{3,5}$ | Joist | 2,650 | 2,200 |
|  | Plank | 3,300 | 2,400 |
| Tensile strength $\left(F_{\mathrm{t}}\right)^{4}$ |  | 2,450 | 1,550 |
| Longitudinal Shear $\left(F_{\mathrm{v}}\right)$ |  | Joist | 200 |
|  | Plank | 150 | 150 |
| Compression Parallel $\left(F_{\mathrm{c}}\right)$ |  | 2,600 | 2,350 |
| Compression Perpendicular $\left(F_{\mathrm{c}}\right)$ |  | Joist | 850 |
| 80 |  |  |  |

For SI: 1 inch $=25.4 \mathrm{~mm}, 1 \mathrm{psi}=6.89 \mathrm{kPa}$

1) The allowable design stress provided in Table 1 apply to protected, dry service conditions
2) The tabulated allowable design stresses above are permitted to be adjusted for duration of load as provided in the appropriate code sections
3) The tabulated flexural stresses above are permitted to be increased by 4 percent for repetitive member stresses as provided in the applicable code for solid sawn lumber
4) The tabulated tensile stress is based on gage length (L) of 2 feet. For other gage lengths, the tabulated tensile stress is adjusted by multiplying $F_{t}$ by $(2 / L)^{0.08}$ where $L$ is measured in feet. For lengths less than 2 feet use the tabulated tensile stress unadjusted.
5) The tabulated flexural stresses are based on load of normal duration and a reference depth of 12 inches. For other depths, the tabulated flexural stresses are adjusted by a depth size factor adjustment of $(12 / \mathrm{d})^{1 / 7}$ as shown in the table below.

| DEPTH <br> (in) | $\mathbf{3 . 5}$ | $\mathbf{5 . 5}$ | $\mathbf{7 . 2 5}$ | $\mathbf{9 . 5}$ | $\mathbf{1 2}$ | $\mathbf{1 4}$ | $\mathbf{1 6}$ | $\mathbf{1 8}$ | $\mathbf{2 4}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.8 E | 1.20 | 1.12 | 1.08 | 1.04 | 1.00 | 0.98 | 0.96 | 0.94 | 0.90 |
| 2.0 E | 1.20 | 1.12 | 1.08 | 1.04 | 1.00 | 0.98 | 0.96 | 0.94 | 0.90 |

TABLE 2: Ultralam ${ }^{\text {TM }}$ LVL FASTNER DETAILS

| TEST |  | $\begin{aligned} & \text { NEAREST SPP } \\ & \text { COMBINATION } \\ & \text { RECOMMENDED } \end{aligned}$ |
| :---: | :---: | :---: |
| WITHDRAWAL-8d NAIL INSTALLED IN Y DIR. (FACE) | Withdrawal | Red Maple (0.58) |
| WITHDRAWAL-8d NAIL INSTALLED IN X DIR. (EDGE) | Withdrawal |  |
| BEARING-10d NAIL INSTALLED IN Y-DIRECTION | Loaded in L-Dir. | Westem White Pine(0.40) |
|  | Loaded in X-Dir. |  |
| BEARING-10d NAIL INSTALLED IN X-DIRECTION | Loaded in L-Dir. |  |
|  | Loaded in Y-Dir. |  |
| BEARING-Loaded in L-Dir. (Parallel) | $1 / 2^{\prime \prime}$ BOLT | Red Maple (0.58) |
|  | 3/4" BOLT |  |
| BEARING-Loaded in X-Dir. (Perpendicular) | 1/2" BOLT | Red Pine (0.44) |
|  | 3/4" BOLT |  |

Allowable values for nails noted in the applicable code are applicable to the Ultralam ${ }^{\text {TM }}$ LVL for conditions and species noted in the table.

